

# The path for innovative severe accident neutronics studies in ZPRs. Part I.1 - Analysis of SNEAK-12A experiments for core disruption in LMFBRs



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## ABSTRACT

The present work details a new benchmark to be produced to the International Community, for dealing with neutronics code validation in the frame of the analysis of severe accidents in Sodium Fast Reactors (SFRs) leading to core degradation and material relocation. The benchmark is based on analysis of selected experiments performed at the Schnelle Null-Energie-Anordnung Karlsruhe (SNEAK). The SNEAK-12A experiments have been considered where core distorted configurations have been simulated. In the paper, the experimental results have been analyzed by using TRIPOLI-4, MCNPX2.7, and Serpent-2 Monte Carlo codes as reference tools, and the ERANOS system of codes for deterministic calculations, all based on JEFF-3.1.1 nuclear data libraries. The complete material balance, and the main degradation sequences are provided within the manuscript. Preliminary results on available experimental results ( $k_{\text{eff}}$ ) are given, and additional local quantities are calculated, such as axial flux distributions, as well as detector responses as function of the distance to the degraded part. The benchmark offers an excellent opportunity to validate calculation schemes for strongly heterogeneous interfaces, in particular the preparation of homogenized self-shielded neutron cross-sections for deterministic core calculations, as well as leakage treatment in locally very heterogeneous media. This work is done within the frame of new core design capacities and new ways of conducting experiment in Zero Power Reactors, such as the ZEPHYR project led independently by CEA. The present analysis will be completed by a full nuclear data sensitivity and uncertainty analysis of the reactivity coefficients and  $k_{\text{eff}}$  in a companion paper.

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## 1. Introduction

Severe Core Accident (SCA) in Liquid Metal-cooled Fast Breeder Reactors (LMFBRs) could occur either due to prompt or super-prompt recriticality or serious loss of heat sink (Ninokata et al., 1995). The progression of a SCA in Fast Breeder Reactors (FBRs) is significantly influenced by the core physics, which is the primary focus of the SNEAK-12A experimental series (Helm and Henneges,

1985; Henneges, 1988; Maschek et al., 2005), since the core is not assembled in its most reactive configuration. Redistribution processes of core materials (fuel, sodium, absorbers, or structural materials) may potentially lead to recriticality events and severe power excursions. Therefore, the study of SCA progression requires an adequate description of the core's neutronic behavior during the different stages of the SCA. Reactivity changes in the core could result from many different reasons, whereas the main contributors are:

- (1) Loss of coolant - this type of accident leads to neutron spectrum hardening and increased neutron leakage.
- (2) Change in material arrangement - could either increase or decrease neutron streaming.

Acronyms: SNEAK-12A, Schnelle Null-Energie-Anordnung Karlsruhe 12A; CDA, Core Disruptive Accident; FBR, Fast Breeder Reactor; LMFBR, Liquid Metal-cooled Fast Breeder Reactor; SCA, Severe Core Accident; TMI, Three Mile Island; ZEPHYR, ZEPHYR power PHYSics Reactor; ZPR, Zero Power Reactor.

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- (3) Redistribution of fuel and structural materials - could lead to streaming effects and changes in the neutron direct and adjoint fluxes.
- (4) Accumulation of relocated fuel in certain regions of the core - could lead to an increase in the core multiplication factor.

These phenomena may have pronounced influence on the neutronic characteristics of the core, which could severely damage both normal and emergency operation of the reactor. Therefore, in order to predict the core behavior during such disruptions, it is imperative to develop accurate and precise computational and experimental tools and methodologies for studying these phenomena. Furthermore, the validation of computational tools against experimental measurements of critical assemblies that represent different stages of the disrupted core configurations is mandatory for evaluating the code performances and quantify any discrepancies between experiment and theory.

This paper presents a new benchmark problem based on the SNEAK-12A critical assembly experiments (Helm and Henneges, 1985; Henneges, 1988) performed in the '80 s at the Schnelle Null-Energie-Anordnung Karlsruhe (SNEAK), (i.e. Fast Zero-Power Facility Karlsruhe), located at Kernforschungszentrum Karlsruhe (KFK), now renamed Karlsruhe Institute of Technology (KIT) and was primarily used for analyzing the neutronics in different fast reactor core configurations and for studying the reactivity effects of material relocation in such systems. During the program, several neutronic codes, such as SNOW (Guenther and Kinnebrock, 1973), TP2 (Kobayashi, 1979), and the neutronic solver of SIMMER-II (Maschek et al., 2005) were validated against the experimental program results.

It should be noted that the course of events during a hypothetical core disruptive accident in fast reactors, e.g., an unprotected loss of flow (ULOF), is usually described in several phases (Riyas and Mohanakrishnan, 2014; Suzuki et al., 2015). Each phase is characterized by a set of physical phenomena. The initial phase of a ULOF deals with the loss of coolant flow (e.g., pump coastdown, main steam line break, etc.) and the subsequent processes that lead to the primary power excursion. This power excursion, if important enough, can initiate local sodium voidage, and hence first local fuel melt. The process initiates material redistribution processes, which start a few seconds after the first melt formation. The neutronics codes used for modeling this accident phase are mainly based on multigroup diffusion approximation, point kinetics model, and first order perturbation calculations (however, some code do allow better approximations, i.e. SIMMER). These approximations are valid as long as in-core material redistribution processes have not yet begun. However, as the SCA progresses into the next phase, where thermal-hydraulics conditions reach their heat transfer limits and gravity acts on molten core materials, the spatial distribution of the neutron flux is dramatically changed, and space-dependent kinetics is required for adequate neutronic modeling of this phase.

The accidents at Chernobyl, Tree Mile Island (TMI-2) and, more recently, at Fukushima, allow to better understand a realistic core behavior during a catastrophic event. Degraded core processes are a key factor in progression of a SCA. An in-vessel accident progression is a non-coherent step-wise process, which results in a melting and liquidation of core materials at different temperatures. In fast reactors, one of the major concerns is a recriticality event due to a core disruptive accident (CDA), in which the reactivity is increased due to fuel redistribution in the core (Ninokata et al., 1995; Sawada et al., 1998), thus causing a power transient. The concern in such an event is that the mechanical energy generated during such a transient would compromise the integrity of the reactor vessel and containment building. The conventional way to ensure the integrity

of the fast reactor is to impose stricter limits on the primary design of the reactor, which are derived from conventional assumptions (e.g. designs include facilities that could withstand large power excursion). Recent research in the sphere of recriticality possibility in fast reactors focus on mechanisms for preventing the possibility of recriticality event sphere (Sawada et al., 1998, 2000; Yamano et al., 2008; Tobita et al., 2007; Konishi et al., 2007), without any reference to recriticality possibility due to the failure of the mechanism.

Recriticality accident is of less concern in LWRs (although molten pool can present, in some geometries, recriticality situations), prompt recriticality is a major issue in modern Gen-IV fast reactor safety studies. As an indicator, all past studies on SCA were performed in fast critical facilities. In particular, fuel melting is an intrinsic danger situation in fast reactors as local void fraction in previous design were characterized by a positive power coefficient, hence leading to excursion. The experimental configurations studied in SNEAK-12A were representative of the second phase of in-core material redistribution of varying sizes.

Several other experiments of core disruption were carried out around the world, e.g., ZEBRA-8G and ZEBRA-12 (Collins and Ingram, 1973), ZPPR-5 (Kaiser et al., 1976), ZPPR-9 (Curtis et al., 1979), and FCA VIII-2 (Nakano et al., 1984). However, among these programs SNEAK-12A was the most comprehensive, with large number of experiments aimed at measuring reactivity changes caused by one of the following: cavities, streaming channels, redistribution of structural material, dispersal and recompaction of fuel, or formation of molten pools at the bottom of the core.

Therefore, there exists an essential need to re-introduce this benchmark problem to the nuclear community, accompanied by advanced state-of-the-art computer codes calculations and additional critical experiments able to bridge the knowledge gap related to core physics phenomenon. As GEN-IV reactors are mainly foreseen to operate in fast spectrum, this benchmark problem could provide additional information regarding core behavior during progression of a SCA in such reactors from a pure neutronics point of view. This revisit of the SNEAK benchmarks is a first step for a future program, aiming to study neutronic behavior of fast reactor core under SCA that would be implemented in the ZEROPower PHYSICS Reactor (ZEPHYR) (Blaise et al., 2016).

## 2. SNEAK-12A- benchmark specification

The information regarding SNEAK-12A core outline is mainly stored in the SNEDAX data base (Helm, 1996). The SNEDAX database contains information on built assemblies and experiments performed in SNEAK (FZK Karlsruhe), MASURCA (CEA Cadarache), ZEBRA (IAEA Winfirth), and RRR (Rossendorf Ringneutronen Reaktor) fast critical facilities. This section provides a short overview of the SNEAK-12A core geometry outline, loaded with uranium fuel plates, as described in Section 2.1. This was mainly dictated by the availability at the time when the experiments were carried out. The basic fuel cell geometry in the SNEAK-12A was designed according to the following requirements –

- (1) Fuel cells should be easily loaded into or unloaded from the core.
- (2) Fuel and sodium densities should be easily determined and updated anywhere in the core (including sodium void formation) for the purpose of material redistribution experiments.
- (3) The core neutronic characteristics should be similar to those of a fast spectrum power reactor.

In the case of the SNEAK-12A core the material volume fractions of the fuel, steel and sodium corresponded approximately to those of the SNR-300 reactor (Helm et al., 1984).

### 2.1. Core description

The SNEAK-12A core consists of horizontal fuel plates assemblies, and is cooled by air, which flows through the gaps between the fuel assemblies. The total core width including unused areas (filled with air) is  $326.4 \times 326.4 \text{ cm}^2$  and total height of about 240 cm. The active region is  $130.56 \times 130.56 \text{ cm}^2$  in area and about 80 cm in height surrounded by 30 cm of upper and lower reflectors, which makes a total of 140 cm. The radial blanket fuel assemblies are slightly longer than the fissile fuel assemblies, leading to a total height of about 150 cm. The core consists of three main radial zones: the radial blanket, the fissile active zone and the test zone that changes from a grid of  $4 \times 4$  to  $6 \times 6$ , as shown in Fig. 1. The core reactivity was controlled by 14 shim rods (marked by blue squares in Fig. 1) located in the core center zone and 6 shim rods located at the core-blanket boundary.

The fuel assembly is a  $5.44 \times 5.44 \text{ cm}$  rectangular filled with horizontal plates of fuel and sodium, with air flowing between them as coolant. A representative fuel assembly is schematically shown in Fig. 2. Most of the fuel assemblies in the core are composed of 35% and 20% enriched uranium metal slabs. The blanket and the axial reflectors consist of depleted uranium dioxide. The full specifications of the SNEAK-12A are given in Appendix A.

### 2.2. Experimental configurations

The SNEAK-12A program included a large number of experiments. However, this benchmark covers only a limited number of experiments, which had the most detailed documentation in the SNEDAX data base. Furthermore, the experiments considered in this benchmark were also chosen according to their potential to create a sequence of configurations which would best represent the events initiated by the SCA phases described above.

The first set of experiments represents a sequence of fuel melt down events (SCA progression), which is initiated by a complete channel voiding. The second stage is a small fuel compaction around the core mid-plane, followed by a large fuel compaction. The last stage is the accumulation of the entire fuel assembly fissile and fertile material content at one end of the core. The different stages are schematically illustrated in Fig. 3. In this work, this sequence was considered on both small scale (4 affected fuel assemblies) and large scale (16 affected fuel assemblies) at the core center. It should be noted that the total material inventory remains constant during the different stages.

The second set of experiments deals with the accumulation of molten material near one of the axial blanket areas. Fuel was compacted asymmetrically near one of the core boundaries and supported by a low density empty steel box, as seen in Fig. 4, in a varying number of affected fuel elements (from 4 to 36) using the same material configuration in all the affected fuel assemblies, as shown in Fig. 5. In the case of the SNEAK core, the fuel compaction was created at the upper plenum due to the core safety features (shim rods where extracted downwards).

## 3. Computational tools

Reactivity calculations for the different configurations studied in this work were performed by Monte Carlo (MC) based codes (MCNPX (Pelowitz, 1999), Tripoli4 (Brun et al., 2015) and Serpent2 (Leppanen et al., 2015)) and by the ERANOS reference deterministic

transport code (Ruggieri et al., 1973). The nuclear data library used in this study is based on the JEFF-3.1.1 evaluation with some comparison made to ENDF-B.VII/1 libraries. For each configuration, a 2D (R-Z) ERANOS model has been assessed, transport calculations being performed by employing the self-shielded neutron cross-section processed at 33 energy groups by means of the ECCO code. This 33-energy mesh, adequate for fast studies, is derived from the international X-MAS 172-energy structure. The MC calculations exact 3-dimensional geometry as specified by the SNEAK-12A benchmark. The calculations are performed based on 200k neutron histories with 500 active and 50 in-active cycles, such as to guarantee a convergence on the  $k$ -eff of less than 10 pcm ( $10^{-5} \Delta k/k$ ) and less than 1% on local flux distributions.

## 4. Results

In this section measured and calculated results are compared. In order to obtain an indication of the accuracy of the different codes, results from all different experimental and theoretical methods are cited.

### 4.1. Clear criticality experiments

The different experiments considered in this section are all referenced to the most basic unperturbed core loading of SNEAK-12A (the reference core). Therefore, it is essential to correctly calculate the reference core. The experimental versus calculated values are summarized in Table 1, where the values on the diagonal are the effective multiplication factor obtained from each code, as the off-diagonal correspond to the relative discrepancies between the different columns (in pcm). It should be noted that the results presented in Table 1 correspond to a core configuration with five edge elements and not seven, as presented in Fig. A.31, where edge elements at position (06,16) and (18,17) should be replaced by a blanket element. However, for the rest of the reactivity effects studies in this paper this edge element is present. As can be seen, there are very small differences between the MC based codes and the experimental value. However, when examining this core in R-Z geometry with ERANOS, the error significantly increases, with an underestimation of the critical state by about 0.6%, as expected from numerous studies. The impact comes mainly from a cylindricalization effect of the - almost-square core, combined with a strong simplification of the shim rod insertion, modeled by an homogenized ring of absorber in the RZ geometry.

Unfortunately, there is almost no available data for comparison except the core effective multiplication factor and the reactivity changes between the different configurations. This is due to lack of miniature measurement equipment that could be fitted in to the tight core arrangement of the SNEAK. Therefore, a presentation of flux traverses and reaction rates distribution is made for code-to-code comparison only. As shown in Fig. 6, there is an excellent agreement between the integrated axial flux distribution along the core center line that where obtained from the different MC codes and between MCNP and ERANOS for the clear criticality configuration.

### 4.2. Molten pool configurations

In this series of experiments, in which the fuel was compacted near one axial blanket area (see Fig. 4), the affected area was radially enlarged in several steps. Initially, the experimentally measured reactivity decreases until reaching a minimal value. For larger radii of the affected area, the reactivity rises and at some point becomes positive, as can be seen in Fig. 7. This reactivity increase is mainly due to the fact that, for smaller radii, the reactivity

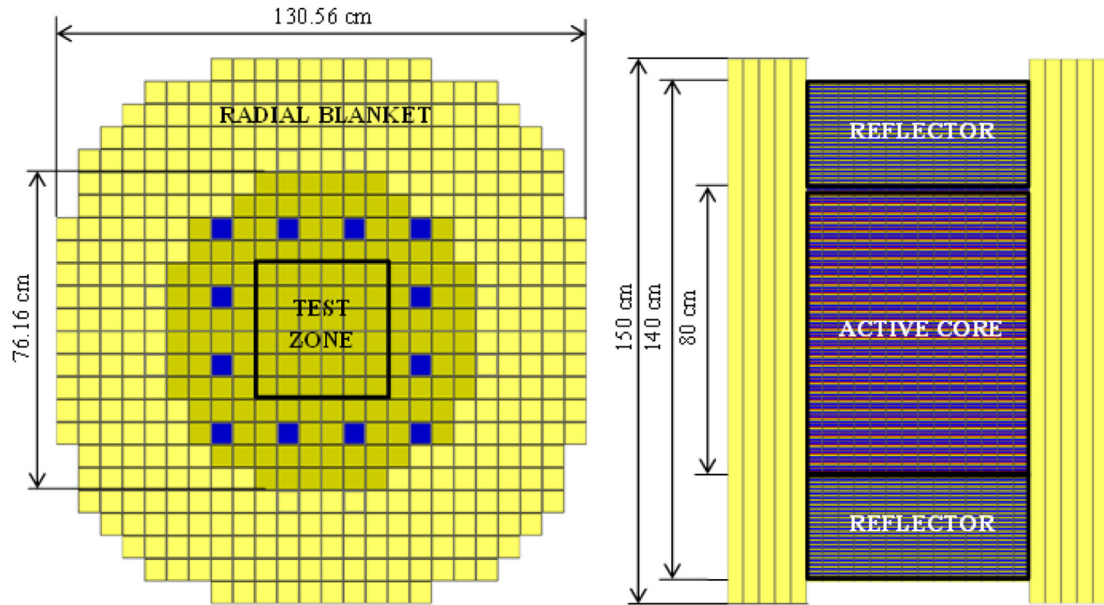


Fig. 1. SNEAK-12A core layout and dimensions. The blue squares indicate on the shim rod positions (left - XY cross section, right XZ cross section).

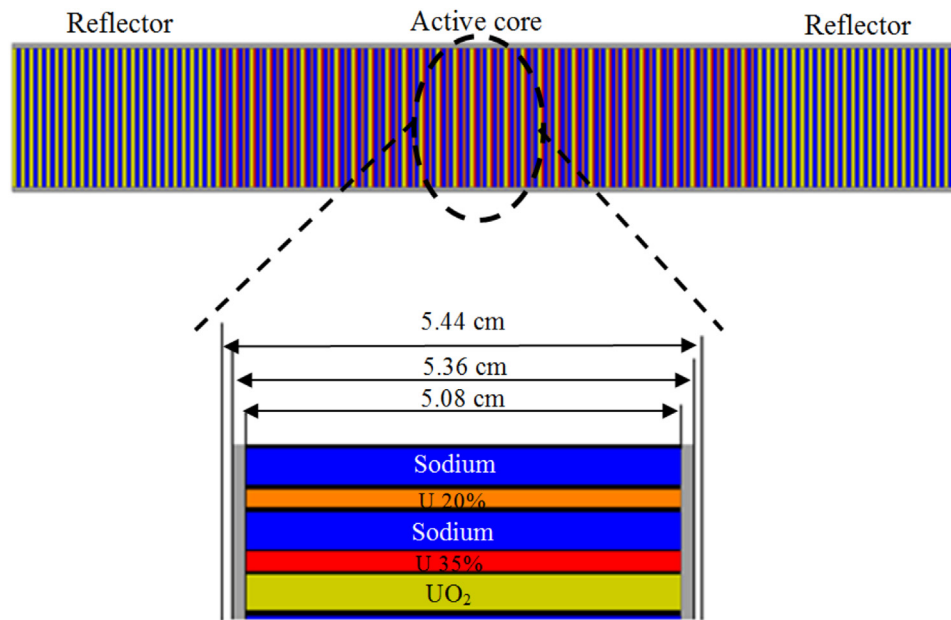


Fig. 2. XZ cross section of a typical fuel assembly geometry and material composition.

changes are mainly governed by the fuel redistribution to regions characterized by lower flux and importance. However, for larger affected area, the increased multiplication in the compacted region predominates.

Fig. 8 show two-dimensional cross sections, calculated by Serpent, of the normalized flux distribution in different stages of the SCA progression. The results shown in Fig. 8 support the claim that the flux shifts towards the compacted region as the molten pool configuration grows larger. Furthermore, a strong impact of the utilized cross-section data is exhibited, where the simulation with the ENDF-B.VII/1 library is slightly underestimates the reactivity changes (Fig. 7). Recent studies on fast systems showed that for some fast assemblies JEFF-3.1.x libraries tend to yield multiplication factors relatively higher in comparison to the same simulation

made with ENDF-B.VII, whereas JEFF-3.2 showed a better agreement on SFR neutronic benchmarks (Aures et al., 2016). However, in the case of SNEAK-12A JEFF-3.2 data yield large discrepancies between the calculated and experimental values of the  $k_{eff}$  of the different experiments. Therefore, it requires a further investigation, which is beyond the scope of the current work. This investigation would be carried out in the near future and proposed to the JEFF community in latter time. It should be noted that the differences seem to be constant and the reactivity changes, calculated with JEFF-3.2 nuclear data, are consistent with the measurements.

As shown in Fig. 7 and summarized in Table 2, the MC codes predict the molten pool growth very well with only a small deviation with respect to the experimental data. The only point with large deviation is the final 36 affected element configuration, which



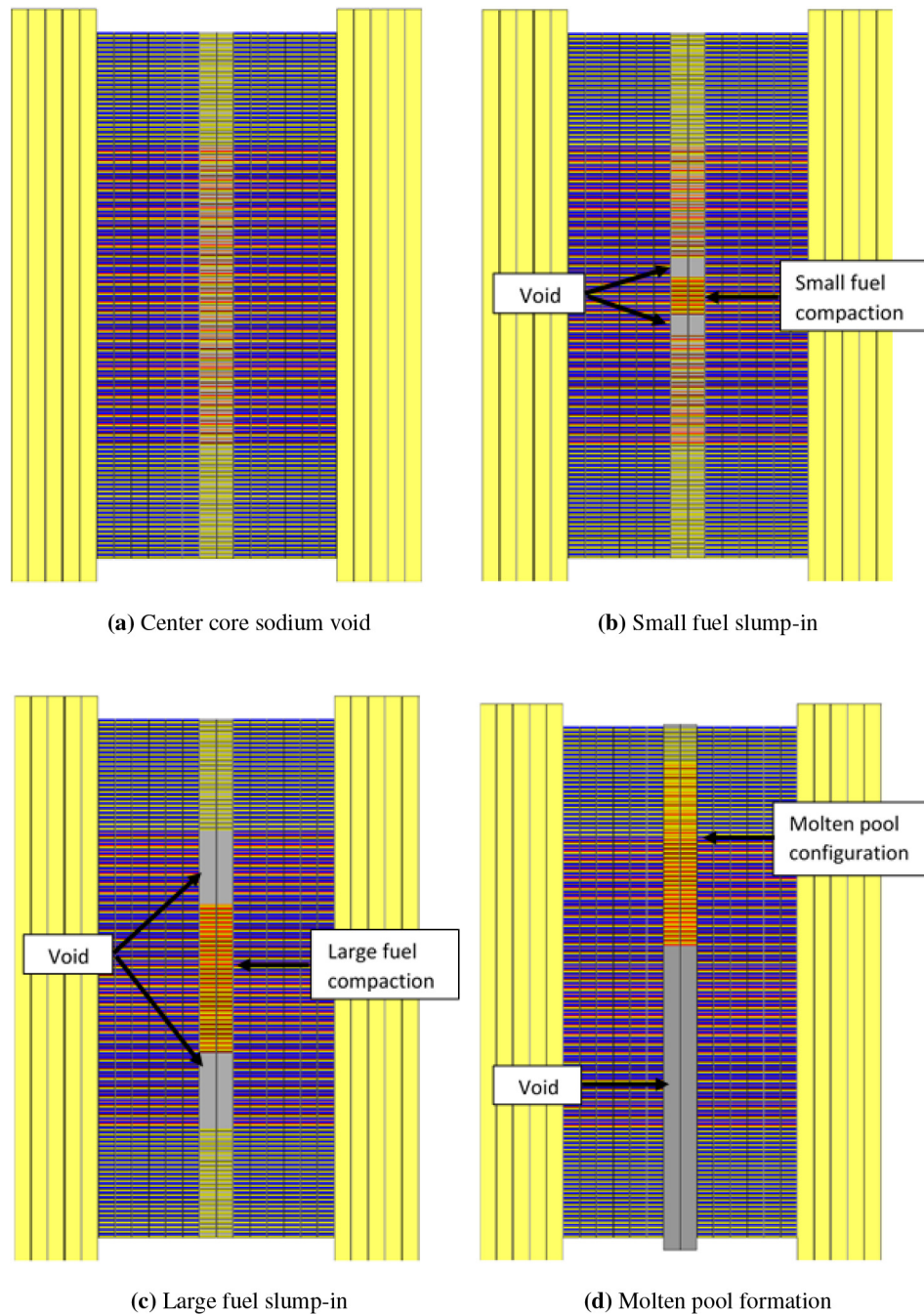


Fig. 3. Different stages of SCA progression in the SNEAK-12A core.

was declared as a calculated point in the SNEDAX data base. Unfortunately, there is no explanation on the calculation methodology, or whether it was obtained from code calculation or extrapolated from the experimental results. The R-Z calculation in ERANOS (star marker in Fig. 7) show a similar behavior to the experimental curve for the small molten pool configurations (4, 12 and 16 affected elements). However, for larger molten pool configurations, specially in the region where the reactivity change becomes positive (above 26 affected elements) ERANOS results constantly over estimate the experiment, with a constantly growing discrepancy. The ERANOS results then exhibit similar behavior observed in the Helm's original SNEAK-12A analysis with SIMMER-II (Helm et al., 1984) transport calculation as seen in Fig. 9.

As shown in Fig. 9, there is a small constant difference between the transport calculations and the experimental results. The diffusion results, on the other hand, are consistently under estimates predictions of the molten pool behavior.

Fig. 10 summarizes axial flux distribution obtained from all codes in the 28 affected elements configuration. As depicted from the results, there is a good agreement between all the MC codes, whereas ERANOS clearly under estimates the flux in the voided region ( $-80 < Z < 0$ ) and over estimates it in the molten pool configuration ( $0 < Z < 80$ ). This might be due to the model uncertainties, which arises from the meshing limitations in the deterministic code. Furthermore, from a large amount of dedicated experimental validation from different sodium void programs

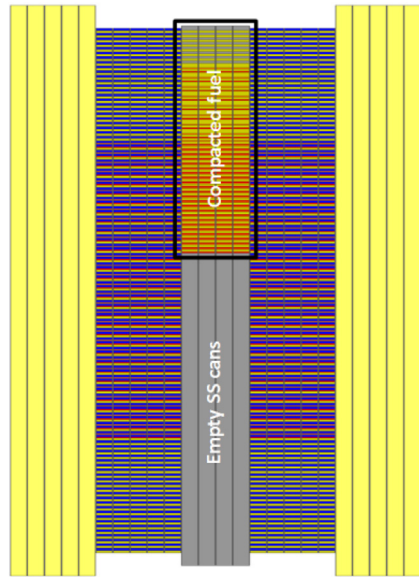


Fig. 4. XZ cross section of a molten pool configuration.

#### 4.3. Fuel slump-in experiments

This section summarizes the reactivity effects due to redistribution of fuel according to the scheme presented in Fig. 3 (no axial symmetry in Fig. 3, only radial). The reactivity changes due to the fuel rearrangement are dominant by neutronic effects, which influence the sequence of events in the case of a postulated accident.

The small slump-in (Fig. 11 and Table 3) induces a positive reactivity insertion in comparison to the sodium voiding stage. However, the total reactivity remains negative due to the small amount of compacted fuel. On the other hand, the large center core slump-in (Fig. 12 and Table 4) induces a relatively large reactivity insertion, mainly due to large fuel compaction, which reduces the leakage and creates an area of high neutron importance in the core center. The last stage in the small core distortion (Fig. 11) is the molten pool formation, where the reactivity insertion is negative due to relatively small fuel removal from the high importance region in the core center. The same trend is observed on large scale SCA (Fig. 12). This behavior is similar to the one demonstrated in the molten pool formation analysis (see Section 4.2), where 16 molten pool elements induced the most negative reactivity change, as shown in Fig. 7.

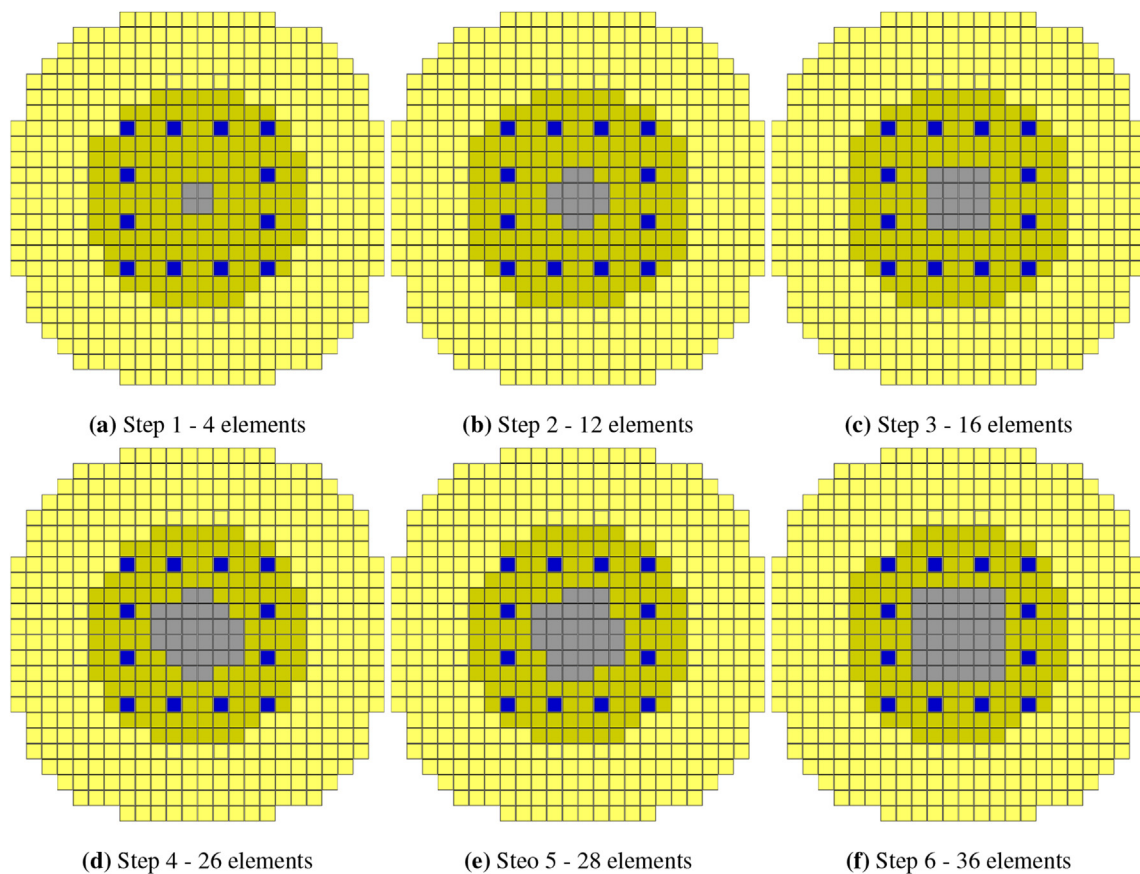


Fig. 5. Different stages of molten pool formation.

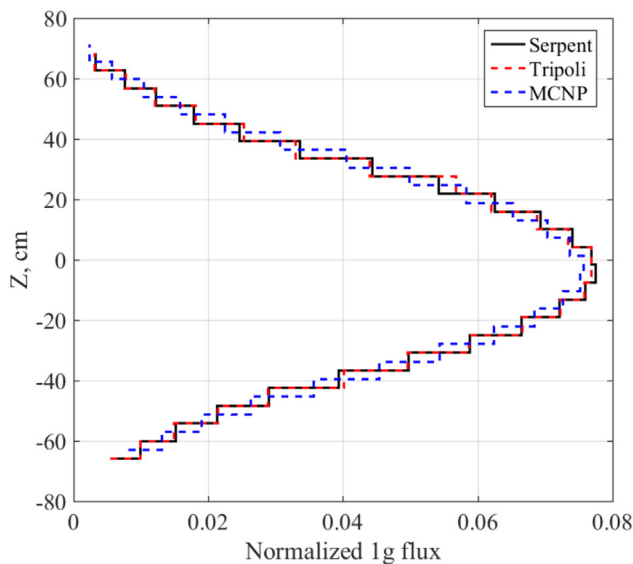
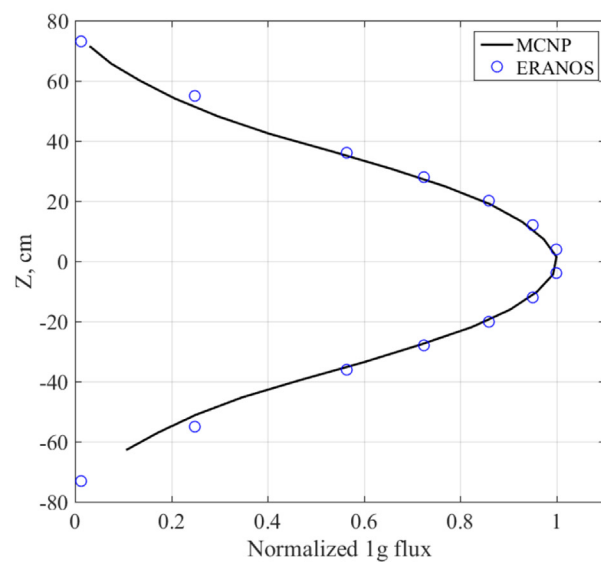
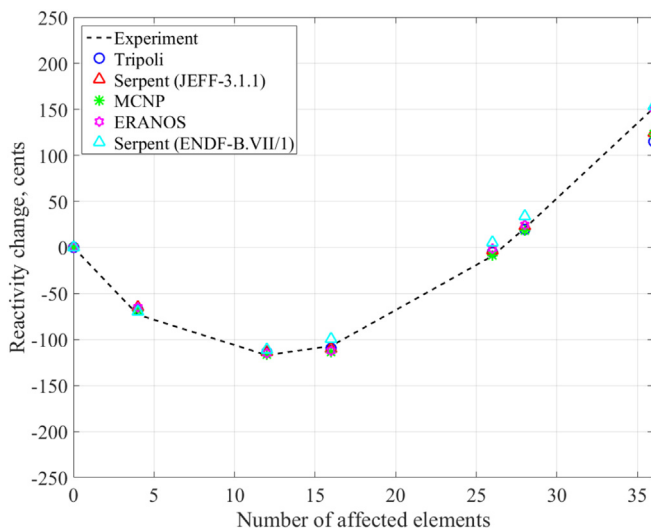
(Tommasi et al., 2010), ERANOS is known to slightly underestimate the leakage factor in sodium void patterns. The MCNP results fit close to the other MC codes with some deviation, resulting from a slight shift in the geometrical mesh.

The relatively large difference between the MC codes and the experimental data at the large slump-in stage for the large configuration (Fig. 12) is a result of different number of affected elements. The experiment at this stage was performed with 12 affected elements while the simulation were performed with 16 affected elements. It was not possible to carry out such and

**Table 1**

Comparison of effective multiplication factor obtained from the experiment and the codes for the basic unperturbed configuration of SNEAK-12A

Source	$k_{\text{eff}}$ value	Deviation from experiment, pcm
Experimental	1.00075	—
Serpent2 (JEFF-3.1.1)	$1.00106 \pm 7.6E-05$	–31
Serpent2 (ENDF-B.VII/1)	$0.99985 \pm 7.6E-05$	90
Tripoli4 (JEFF-3.1.1)	$1.00105 \pm 8.6E-05$	–30
MCNPX2.7 (JEFF-3.1.1)	$1.00167 \pm 1.8E-04$	–91
ERANOS (R-Z)	0.99478	600

**(a)** Comparison of MC codes**(b)** Comparison of MCNPX2.7 vs. ERANOS**Fig. 6.** Comparison of integrated axial flux distribution at core center line obtained by different codes.**Fig. 7.** Reactivity versus number of affected elements in the core center.

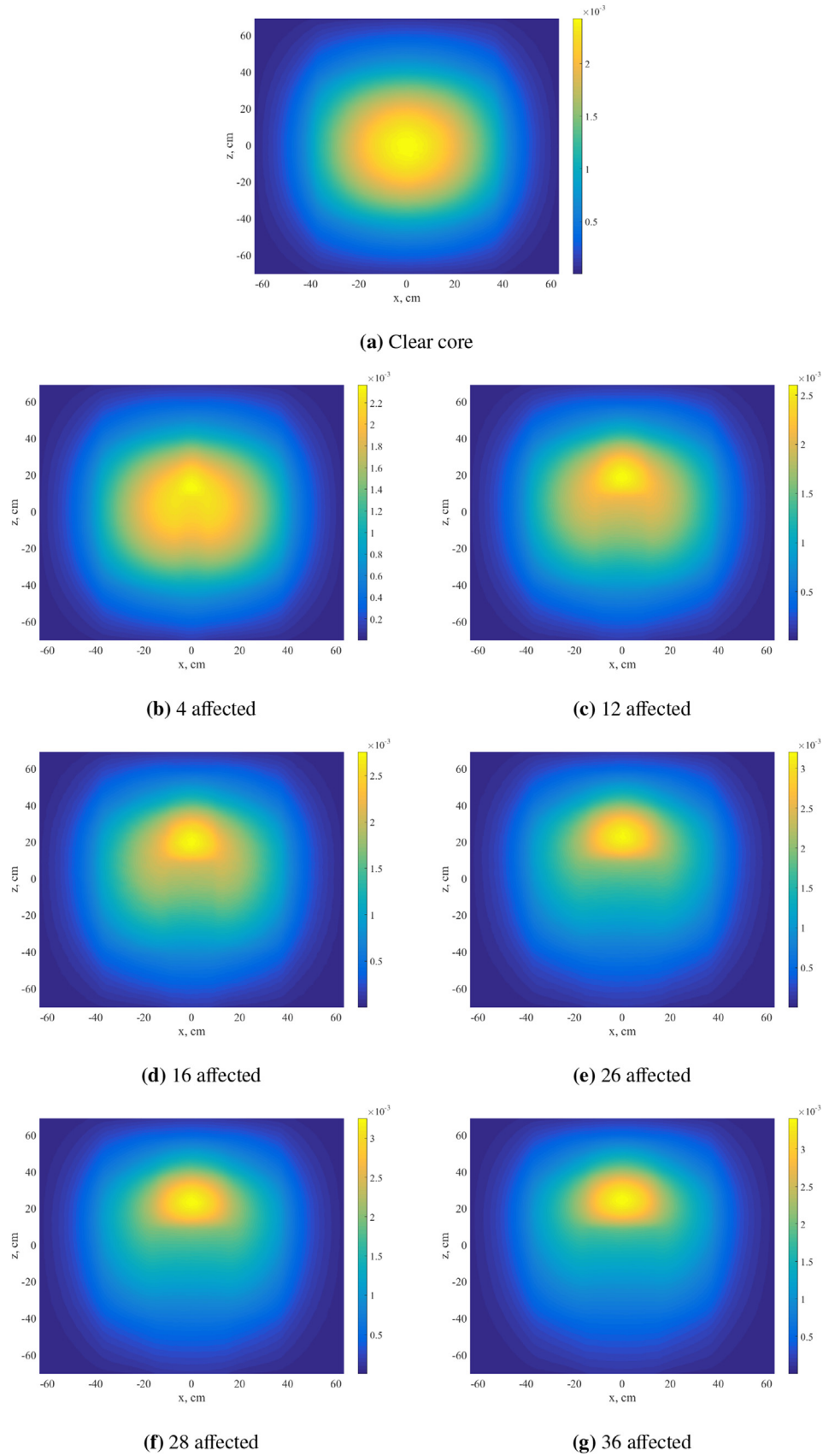
experiment due to very high reactivity insertion that was followed by the fuel compaction in 16 fuel elements. The goal of this section was to maintain the same size of affected region in order to follow a scenario of the same magnitude. However, the results for the 12

affected elements are shown in Fig. 12b, and next to the 16 affected values for large slump-in in Table 4.

The experimental results support several international studies (Kondo et al., 1985; Kayser and Cadarache, 2000; Tobita et al., 2008) regarding elimination of recriticality possibility in LMFBFR reactors, e.g., the Fuel subAssembly with Inner Duct Structure (FAIDUS), studied at the Japan Atomic Energy Agency (JAEA) and the Tokyo Institute of Technology (TIT) (Sawada et al., 1998, 2000; Konishi et al., 2007; Tobita et al., 2008), as well as the CAPRA/CADRA studies on fast burner reactors at CEA Cadarache (Vasile et al., 2000). All these programs focused on techniques or technological innovative assembly designs for avoiding the high reactivity insertion during the molten pool formation (shown in Fig. 7) via the immediate removal of the melted fuel from the core center to the lower or upper plenums, and then to the core catcher.

#### 4.4. Monitoring of SCA progression

The prompt detection of early stages of SCA is of up most importance in terms of reactor safety. The sequence of operations to mitigate SCA is dictated by the stage of the accident progression. Therefore, it is essential to determine the SCA initiation point. Unfortunately, during the operation of the SNEAK-12A program, a dedicated detection methodology was not investigated thoroughly due to both technological drawbacks and tight lattice configurations that did not allow the insertion of adequate miniature detector system inside the core. Simulation of ex-core detectors



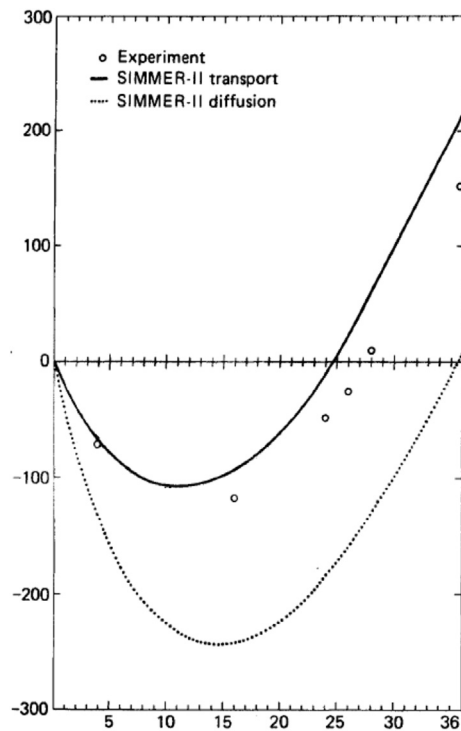
**Fig. 8.** 2D center core axial flux shift due to fuel relocation in molten pool formation.



**Table 2**

Comparison of reactivity changes between different molten pool configurations obtained from the experiment and the codes.

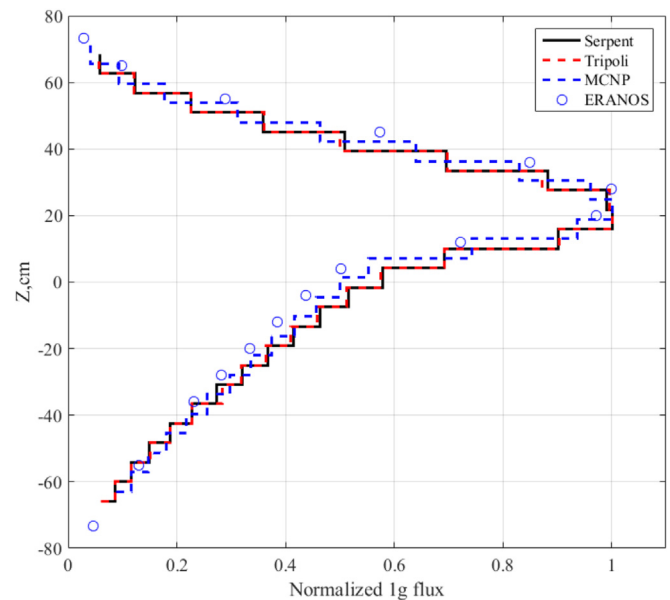
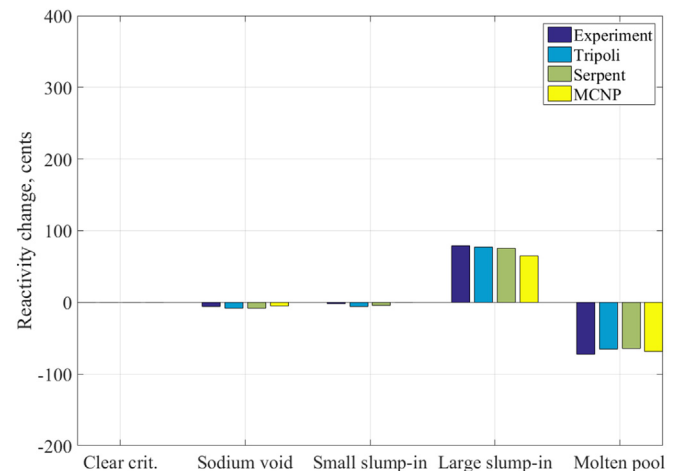
Affected elem.	Experimental	TRIPOLI4	Serpent2	MCNPX2.7	ERANOS(R-Z)
0	0	0	0	0	0
4	-73.1	-67.6 ( $\pm 6.4E-05$ )	-65.0 ( $\pm 5.6E-05$ )	-68.5 ( $\pm 1.3E-04$ )	-65.1
12	—	-113.6 ( $\pm 6.1E-05$ )	-113.6 ( $\pm 5.2E-05$ )	-114.7 ( $\pm 1.6E-04$ )	-115.2
16	-107	-109.6 ( $\pm 6.7E-05$ )	-106.6 ( $\pm 6.0E-05$ )	-120.6 ( $\pm 1.2E-04$ )	-112.80
26	-9.4	-5.3 ( $\pm 6.0E-05$ )	-3.3 ( $\pm 5.9E-05$ )	-8.9 ( $\pm 1.6E-04$ )	-1.46
28	20.6	19.8 ( $\pm 6.1E-05$ )	22.9 ( $\pm 5.4E-05$ )	17.2 ( $\pm 1.6E-04$ )	24.6
36	151.3	115.1 ( $\pm 6.3E-05$ )	124.8 ( $\pm 5.1E-05$ )	123.1 ( $\pm 1.4E-04$ )	234.75

**Fig. 9.** Reactivity versus number of affected elements in the core center computed by SIMMER-II (Helm et al., 1984).

(outside the large blanket region) indicated that it is impossible to derive any meaningful conclusions due to very small neutron leakage rate resulting in poor detector's count rate. In this section, we study a possible solution for early detection of SCA by using in-core detectors, e.g., miniature fission chambers. It should be noted that this part was carried out by Serpent simulation.

In order to be able to predict the behavior of the molten pool configuration, a series of miniature fission chambers were placed in different places on the blanket-core boundary, as shown in Fig. 13. Most of the samplings were made at the shim rods location, which are smaller than the normal core fuel assemblies. Furthermore, location 1 in Fig. 14 and 15 contained two miniature fission chambers, one located at the top end of the active core zone and the second at core mid-plane. For the simulation, two types of miniature fission chambers were considered,  $^{235}\text{U}$  and  $^{242}\text{Pu}$ . The use of  $^{242}\text{Pu}$  as fission chamber deposit is known as being the best choice for monitoring fast neutrons in a high neutron flux (Filliatre et al., 2008).

The detectors in Fig. 13 correspond to the presented results in Figs. 14 and 15 in the following manner -

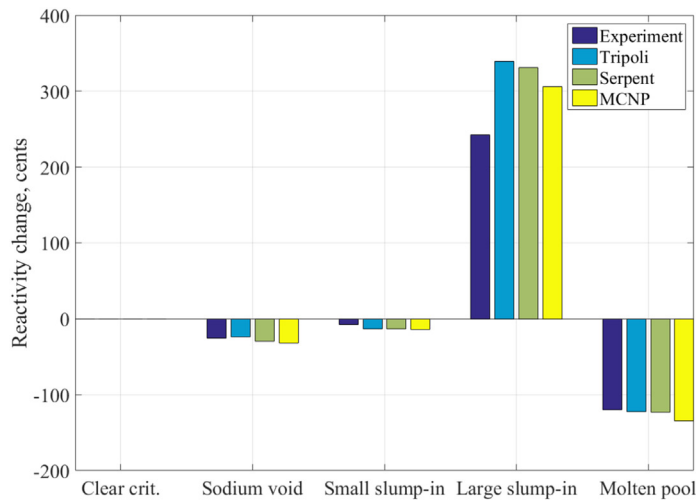
**Fig. 10.** Center line axial flux distribution for 28 affected elements. A comparison between different codes.**Fig. 11.** Reactivity changes due to SCA progression for small affected region.

- Location 1 - This location corresponds to two detectors presented in Figs. 14 and 15, the "Center in" and the "Center in top" detectors. Those detectors located one above the other on the boundary between the fissile inner core and the fertile blanket.

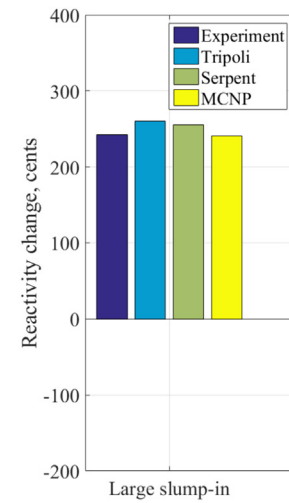
**Table 3**

Comparison of reactivity changes between different small scale SCA progression configurations obtained from the experiment and the codes.

Configuration	Clear	Sodium void	Small slump-in	Large slump-in	Molten pool
Exp.	0	−5.9	−1.4	79.1	−72.2
Tripoli	0	−8.5 ( $\pm 6.0E-05$ )	−5.8 ( $\pm 6.1E-05$ )	77.1 ( $\pm 6.7E-05$ )	−65
Serpent	0	−8.1 ( $\pm 6.1E-05$ )	−4.6 ( $\pm 5.5E-05$ )	75.9 ( $\pm 5.8E-05$ )	−64.5
MCNP	0	−4.7 ( $\pm 1.6E-04$ )	0.02 ( $\pm 1.5E-04$ )	65 ( $\pm 1.4E-04$ )	−68.5



(a) All 16 affected



(b) Just 12 affected

**Fig. 12.** Reactivity changes due to SCA progression for large affected region.**Table 4**

Comparison of reactivity changes between different large scale SCA progression configurations obtained from the experiment and the codes.

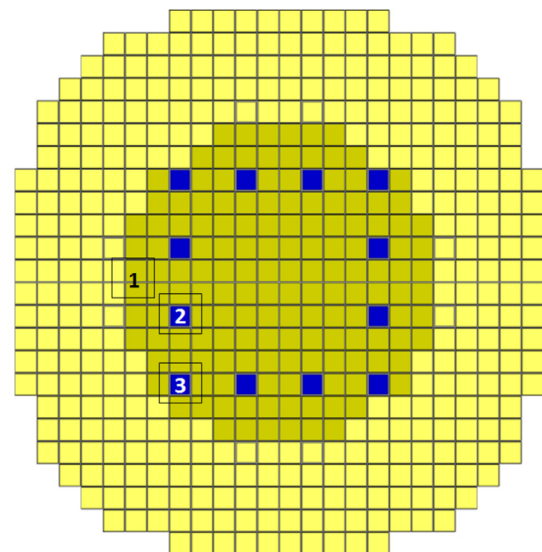
Configuration	Clear	Sodium void	Small slump-in	Large slump-in	Molten pool
Exp.	0	−25.6	−7.4	242.3	−120
Tripoli	0	−23.5 ( $\pm 6.4E-05$ )	−13.2 ( $\pm 6.5E-05$ )	339.1 (260.5) ( $\pm 6.6E-05$ )	−122.5
Serpent	0	−29.8 ( $\pm 6.0E-05$ )	−12.9 ( $\pm 5.8E-05$ )	331 (255.1) ( $\pm 5.6E-05$ )	−123
MCNP	0	−31.9 ( $\pm 1.4E-04$ )	−14.1 ( $\pm 1.7E-04$ )	306.1 (241.1) ( $\pm 1.3E-04$ )	−134.61

- Location 2 - This location corresponds to the "Center mid." detector name in Figs. 14 and 15, located at the gap between the normal core fuel assembly and a shim rod.
- Location 3 - This location corresponds to the "Diagonal in" detector name in Figs. 14 and 15, this detector is located at the diagonal shim rod position.

The fission reaction rates in the different detectors are summarized in Figs. 14 and 15. Two distinct trends of the fission chambers behavior are pointed out. The fission rates in all detectors located at mid XY plane are monotonically decreasing, whereas the top end plane detector exhibits monotonic rise in fission reaction rate. Furthermore, the gradient of the fission reaction rate curve exhibited by the top end plane detector is steeper than that of the mid plane fission chambers. This behavior could be used as indication of the molten pool (or fuel melting) growth.

## 5. Conclusions

The SNEAK-12A program was aimed at validating the neutronics calculation methods for severe accident degraded configurations representative of FBRs. The accident analyses were carried out by

**Fig. 13.** Hypothetical miniature fission chamber locations in SNEAK-12A core.

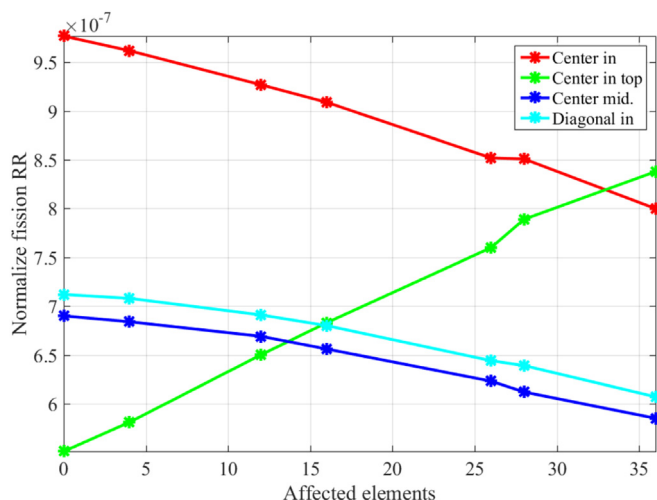


Fig. 14. Fission reaction rates in  $^{235}\text{U}$  detector as function of the number of affected fuel assemblies in molten pool configuration.

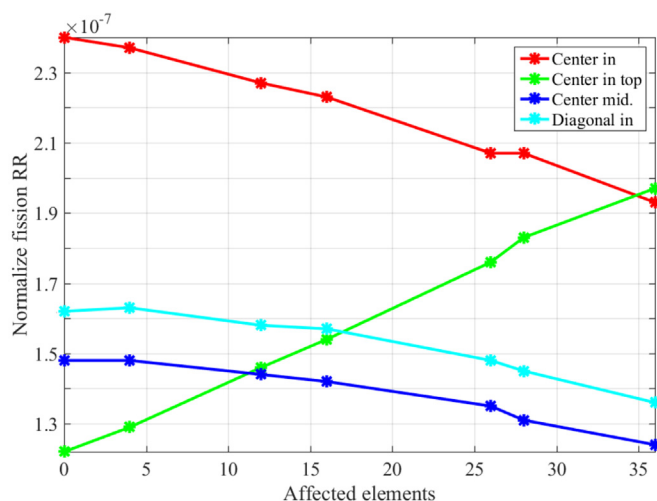


Fig. 15. Fission reaction rates in  $^{242}\text{Pu}$  detector as function of the number of affected fuel assemblies in molten pool configuration.

measurements and calculations of reactivity changes as a results of disturbed core configurations, representing relocation of important materials (fuel, sodium, steel, aluminum) that could occur in the course of accident progression. The data obtained from the SNEDAX data base is presented in this paper in the form of a Monte Carlo codes benchmark problem.

The result of the benchmark showed that the reactivity effects of all unperturbed and distorted configurations could be well predicted by the MC codes - MCNP, Tripoli, and Serpent. The results obtained with the deterministic code ERANOS in R-Z geometry showed a good agreement for small configurations (4 and 12 affected elements), with a larger deviation for larger configuration (28 affected elements). From an extrapolation of those results (Fig. 7) it can be seen that ERANOS over estimates the positive reactivity changes region. This expected behavior is similar to the original SIMMER-II transport calculations performed in the 80's.

The benchmark results represent a solid basis of understanding

in order to study the neutronics behavior of distorted configuration in fast reactor cores. Having this in mind, efforts are going on to carry out similar analyses for other fast reactor systems.

Since SNEAK-12A was loaded with enriched uranium fuel whereas future GEN-IV reactors would operate with plutonium fuel loading, there is a need to validate the neutronic phenomena and reactivity effects, presented in this study, under suitable conditions. Such work is underway with the SNEAK-12B experimental program where the core was loaded with plutonium fuel.

In the last part of this study, we suggested a possible methodology for early detection of severe accident progression and molten pool formation. This subject is of utmost importance regarding the safety of fast reactors and requires further investigation and detailed study. The results presented in this study constitute a "proof of concept" for the suggested early detection and monitoring methodology that should be applied for monitoring core behavior in the course of a SCA.

As mentioned above, a new benchmark based on the SNEAK-12B is currently under investigation. However, the examination of the SNEAK-12A program has not been finished, and further analysis is currently underway, which includes sensitivity analysis of the core reactivity coefficients and associated nuclear data propagated uncertainties. The complete results will be presented in a companion paper. This is a necessary research for future experimental programs to be proposed at CEA Cadarache, in particular in awaited innovative ZPR designs such as the ZEPHYR project lead by CEA.

## Acknowledgment

The authors would like to extend their gratitude to Dr. Gerald RIMPAULT, CEA Cadarache, for providing additional information regarding the operated experiments in the SNEAK facility.

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## AppendixA. Benchmark full specification

This appendix brings the detailed specification of the different fuel assemblies loaded in to the SNEAK-12A core. The benchmark specifies three different levels of geometries. The first is the platelet, this is the most basic geometry and it consists of one plate. The second level is the cell, which is a combination of several platelets. The last level of the geometry is the assembly. An assembly is a combination of multiple cells stacked in a vertical grid. An example was shown in Fig. 2. All the fuel cells have the same basic X-Y cross section, the platelet is  $5.08 \times 5.08 \text{ cm}^2$ , the cladding width is 0.28 cm with the remaining 0.08 cm occupied by air, making the total assembly X-Y cross section to be  $5.44 \times 5.44 \text{ cm}^2$ . For the smaller platelets loaded in the shim rods assemblies the cross section is  $4.68 \times 4.68 \text{ cm}^2$  loaded in to a 0.68 cm thick can, when the outer region filled by air up to the total assembly X-Y cross section  $5.44 \times 5.44 \text{ cm}^2$ .

### AppendixA.1. Assembly 12A-11-01-Radial blanket assembly

The radial blanket consists purely of depleted uranium. The assembly axial cross section is shown in Fig. A.16 with the dimensions given in Table A.5 and material balance in Table A.6.

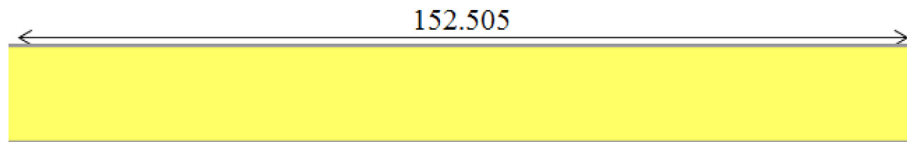


Fig. A.16. Axial cross section of blanket fuel assembly.

Table A.5

Assembly 12A-11-01 cell boundaries and platelets quantities.

Cell	From, cm	To, cm	Num. of ele.	ele. height, cm
BL- UDEPL1	−76.2526	76.2526	5	30.501

Table A.6

Assembly 12A-11-01 material balance, #/ cm b.

Isotop	BL-UDEPL1
Ni	4.727237E-04
<sup>235</sup> U	1.862878E-04
<sup>238</sup> U	4.580126E-02

Table A.8

Assembly 12A-10-01 platelets boundaries.

Plate	From, cm	To, cm	ele. height, cm
Cell A			
UO2 NP6	0	0.6257	0.6257
U 35% NP3	0.6257	0.9401	0.3144
NATRIUM NP6	0.9401	1.5649	0.6248
U 20% NP6	1.5649	1.8799	0.3150
NATRIUM NP6	1.8799	2.5047	0.6248
Cell B			
UO2 NP6	0	0.6257	0.6257
NATRIUM NP6	0.6257	1.2505	0.6248

Table A.9

Assembly 12A-10-01 material balance, #/ cm b.

Isotop	UO2 NP6	U35% NP3	NATRIUM NP6	U20% NP3
Al	1.380427E-05	—	—	—
C	6.399417E-05	—	4.371840E-04	—
Cr	1.944067E-03	—	3.584877E-02	—
Fe	6.886453E-03	—	1.259854E-01	—
H	1.765199E-05	—	—	—
Mg	6.123131E-06	—	—	—
Mn	4.007326E-05	—	6.832343E-04	—
Mo	1.126957E-05	—	2.621876E-04	—
Na	—	—	3.082528E-01	—
Nb	5.553869E-07	—	—	—
Ni	1.018455E-03	8.092385E-04	2.369649E-02	8.077022E-04
O	3.990924E-02	—	5.707915E-06	—
P	2.768817E-05	—	1.830844E-03	—
S	1.054332E-06	—	5.586765E-05	—
Si	8.818426E-05	—	2.159033E-02	—
<sup>235</sup> U	1.432592E-04	1.689311E-02	—	9.292719E-03
<sup>238</sup> U	1.975188E-02	3.001687E-02	—	3.706167E-02

#### Appendix A.2. Assembly 12A-10-01 - Normal core assembly

The normal core assembly is a complex assembly made to simulate interactions between the fuel and the sodium, shown in Fig. A.17. Therefore, plates of enriched fuel, to level of 35% and 20%, were separated by solid sodium plate (Natrium), as it can be seen in Fig. A.18a. The assembly is reflected by an axial reflector, which consists of sodium and natural UO<sub>2</sub>, as can be seen in Fig. A.18b. The quantities and the axial dimensions of the cells and the composing platelets is summarized in Table A.7 and Table A.8, where Table A.9 contains the material compositions of all the different platelets.

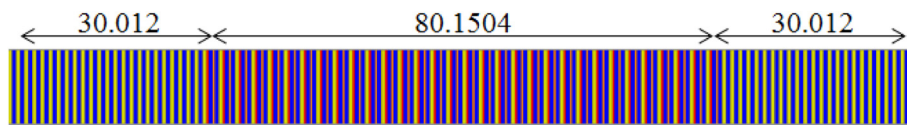
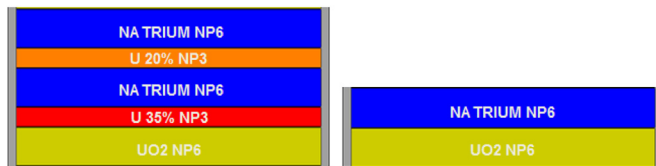


Fig. A.17. Axial cross section of normal core assembly



(a) Cell A

(b) Cell B

Fig. A.18. Composing cells of assembly 12A-10-01.

Table A.7

Assembly 12A-10-01 cell boundaries and platelets quantities.

Cell	From, cm	To, cm	Num. of ele.	ele. height, cm
B	−70.08	−40.08	24	1.2505
A	−40.08	40.08	32	2.5047
B	40.08	70.08	24	1.2505

#### Appendix A.3. Assembly 12A-10-90 - Edge element assembly

Assembly 12A-90-10 only modification in respect to assembly 12A-10-01 is in the axial blanket assembly, as it can be seen in Fig. A.19 and Fig. A.20. The difference in the material composition is not that substantial. However, in order to achieve higher accuracy of the calculations it was not neglected. Table A.10 and Table A.11 summarize the amounts of each platelets and cells in the fuel assembly and their boundaries, where Table A.12 contains the material balance.



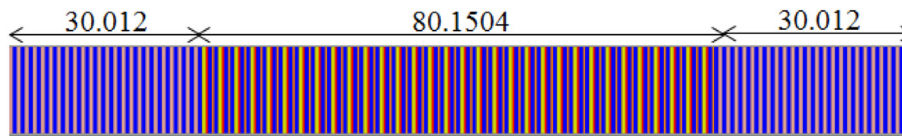


Fig. A.19. Axial cross section of edge element assembly.

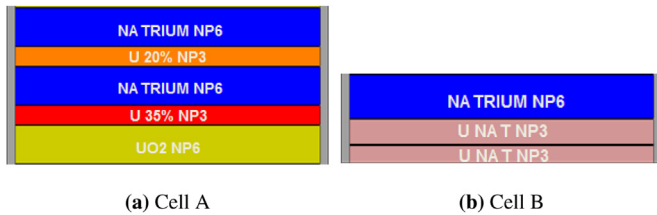


Fig. A.20. Composing cells of assembly 12A-10-90.

## Appendix A.4. Assembly 12A-12-01 - Core center region shim rod

The shim rods in the SNEAK core are made of a fissile material, therefore their insertion brings a positive reactivity feedback. As it was mentioned earlier, the X-Y cross section of the shim rods differs from the X-Y cross section of the fuel elements. Each shim rod has a  $4.68 \times 4.68 \text{ cm}^2$  cross section. The geometry of the core shim rod shown in Fig A.21 and A.22, and dimensions summarized in Table A.13 and A.14. The material balance is summarized in Table A.15.

Table A.10

Assembly 12A-10-90 cell boundaries and platelets quantities.

Cell	From, cm	To, cm	Num. of ele.	ele. height, cm
BM	−70.08	−40.08	24	1.2505
A	−40.08	40.08	32	2.5047
BM	40.08	70.08	24	1.2505

Table A.11

Assembly 12A-10-90 platelets boundaries.

Plate	From, cm	To, cm	ele. height, cm
Cell A			
UO2 NP6	0	0.6257	0.6257
U 35% NP3	0.6257	0.9401	0.3144
Natrium NP6	0.9401	1.5649	0.6248
U 20% NP6	1.5649	1.8799	0.3150
Natrium NP6	1.8799	2.5047	0.6248
Cell BM			
U NAT NP3	0	0.3134	0.3134
U NAT NP3	0.3134	0.6268	0.3134
Natrium NP6	0.6268	1.2505	0.6237

Table A.12

Assembly 12A-10-90 material balance, #/ cm b.

Isotop	UO2 NP6	U35% NP3	Natrium NP6	U20% NP3	U NAT NP3
Al	1.380427E-05	—	—	—	—
C	6.399417E-05	—	4.371840E-04	—	—
Cr	1.944067E-03	—	3.584877E-02	—	—
Fe	6.886453E-03	—	1.259854E-01	—	—
H	1.765199E-05	—	—	—	—
Mg	6.123131E-06	—	—	—	—
Mn	4.007326E-05	—	6.832343E-04	—	—
Mo	1.126957E-05	—	2.621876E-04	—	—
Na	—	—	3.082528E-01	—	—
Nb	5.553869E-07	—	—	—	—
Ni	1.018455E-03	8.092385E-04	2.369649E-02	8.077022E-04	7.991457E-04
O	3.990924E-02	—	5.707915E-06	—	—
P	2.768817E-05	—	1.830844E-03	—	—
S	1.054332E-06	—	5.586765E-05	—	—
Si	8.818426E-05	—	2.159033E-02	—	—
<sup>235</sup> U	1.432592E-04	1.689311E-02	—	9.292719E-03	3.352181E-04
<sup>238</sup> U	1.975188E-02	3.001687E-02	—	3.706167E-02	4.619381E-02

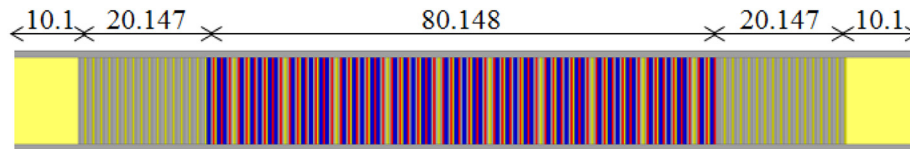


Fig. A.21 Axial cross section of core shim rod assembly.

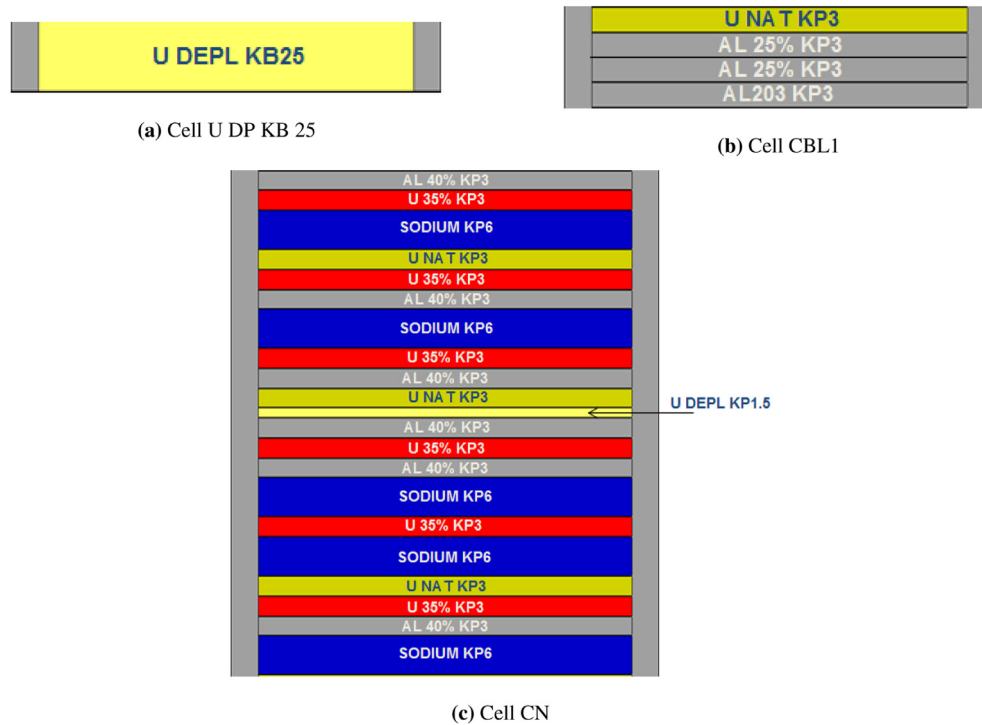


Fig. A.22 Composing cells of assembly 12A-12-01.

**Table A.13**

Assembly 12A-12-01 cell boundaries and platelets quantities.

Cell	From, cm	To, cm	Num. of ele.	ele. height, cm
U DP KB25	−70.08	−60.08	4	2.532
CBL1	−60.08	−40.08	16	1.2592
CN	−40.08	40.08	10	8.0148
CBL1	40.08	60.08	16	1.2592
U DP KB25	60.08	70.08	4	2.532

**Table A.14**

Assembly 12A-12-01 platelets boundaries.

Plate	From, cm	To, cm	ele. height, cm
Cell U DP KB25			
U DEPL KB25	0	2.5320	2.5320
Cell CBL1			
AL203 KP3	0	0.3150	0.3150
AL 25% KP3	0.3150	0.6302	0.3152
AL 25% KP3	0.6302	0.9454	0.3152
U NAT KP3	0.9454	1.2592	0.3138
Cell CN			
SODIUM KP6	0	0.6280	0.6280

**Table A.14 (continued)**

Plate	From, cm	To, cm	ele. height, cm
AL 40% KP3	0.6280	0.9440	0.3160
U 35% KP3	0.9440	1.2574	0.3134
U NAT KP3	1.2574	1.5712	0.3138
SODIUM KP6	1.5712	2.1992	0.6280
U 35% KP3	2.1992	2.5126	0.3134
SODIUM KP6	2.5126	3.1406	0.6280
AL 40% KP3	3.1406	3.4566	0.3160
U 35% KP3	3.4566	3.7700	0.3134
AL 40% KP3	3.7700	4.0860	0.3160
U DEPL KP1.5	4.0860	4.2430	0.1570
U NAT KP3	4.2430	4.5568	0.3138
AL 40% KP3	4.5568	4.8728	0.3160
U 35% KP3	4.8728	5.1862	0.3134
SODIUM KP6	5.1862	5.8142	0.6280
AL 40% KP3	5.8142	6.1302	0.3160
U 35% KP3	6.1302	6.4436	0.3134
U NAT KP3	6.4436	6.7574	0.3138
SODIUM KP6	6.7574	7.3854	0.6280
U 35% KP3	7.3854	7.6988	0.3134
AL 40% KP3	7.6988	8.0148	0.3160

**Table A.15**

Assembly 12A-12-01 material balance, #/ cm b.

Isotop	AL203 KP3	AL 25% KP3	U NAT KP3	SODIUM KP6	AL 40% KP3
Al	4.473958E-02	9.730417E-02	—	—	2.296403E-02
C	—	—	—	3.281205E-05	—
Cr	—	—	—	2.274693E-03	—
Fe	—	—	—	7.948392E-03	—
H	—	—	—	—	—
Mg	1.702613E-04	9.964209E-04	—	—	2.351786E-04
Mn	—	3.528015E-04	—	4.224415E-05	8.325855E-05
Mo	—	—	—	1.734453E-05	—
Na	—	—	—	1.899775E-02	—
Nb	—	—	—	—	—
Ni	—	—	1.343404E-03	1.493208E-03	—
O	6.727969E-02	—	—	—	—
P	—	—	—	—	—
S	—	8.147019E-04	—	4.095983E-06	—
Si	—	—	—	1.481138E-04	1.922626E-04
U235	—	—	3.325779E-04	—	—
U238	—	—	4.580041E-02	—	—
Isotop	U 35% KP3	U DEPL KB25	U DEPL KP1.5	—	—
Ni	9.565251E-04	2.404915E-04	1.819886E-03	—	—
U235	1.689129E-02	1.906997E-04	1.818333E-04	—	—
U238	2.988937E-02	4.688144E-02	4.474099E-02	—	—

**Appendix A.5. Assembly 12A-12-02 - Blanket region shim rod**

The blanket region shim rod consist of a single material, just as the blanket assemblies, shown if Fig. A.23. All the parameters summarized in Tables A.16 and A.17.

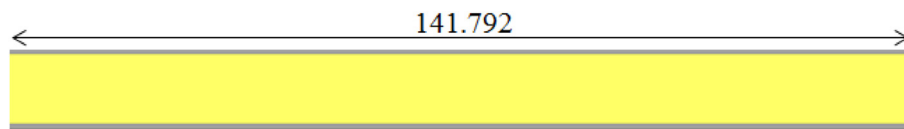


Fig. A.23 Axial cross section of blanket shim rod assembly.

**Table A.16**

Assembly 12A-12-02 cell boundaries and platelets quantities.

Cell	From, cm	To, cm	Num. of ele.	ele. height, cm
U DP KB25	−70.08	71.712	56	2.532

**Table A.17:**

Assembly 12A-12-02 material balance, #/ cm b.

Isotop	U DEPL KB25
Ni	2.404915E-04
<sup>235</sup> U	1.906997E-04
<sup>238</sup> U	4.688144E-02

**Appendix A.6. Assemblies 12A-13-01 and 12A-13-02 - Core's driver and safety rod**

Those assemblies have almost the same distribution of material and geometry as the 12A-12-01 shim rod. The main difference is lower aluminum quantity and sodium presence in the axial blanket. The safety rods in the SNEAK-12A geometry are constantly in their most inner position inside the core. The geometry is show in Fig. A.24 and A.25, and summarized in Table A.18 and A.19. The material balance can be found in Table A.15, this is the same material balance a for the core center region shim rod.

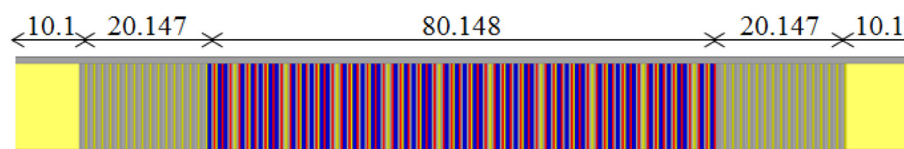


Fig. A.24 Axial cross section of driver and safety shim rods assemblies.

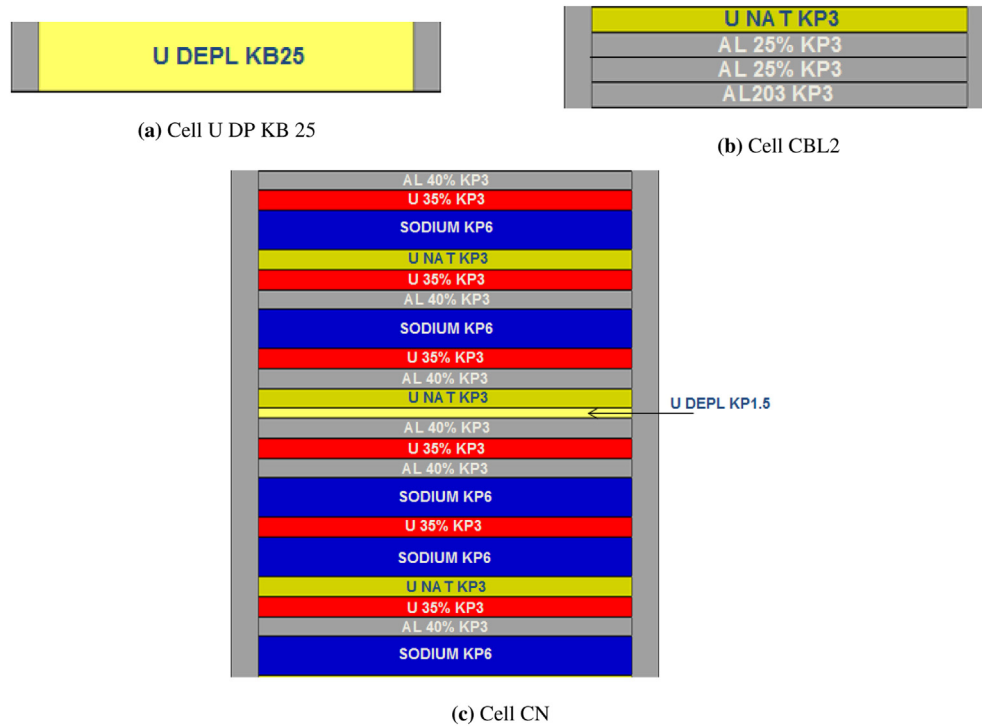


Fig. A.25 Composing cells of assemblies 12A-13-01/2.

**Table A.18**

Assembly 12A-13-01/2 cell boundaries and platelets quantities.

Cell	From, cm	To, cm	Num. of ele.	ele. height, cm
U DP KB25	−70.08	−60.08	4	2.532
CBL2	−60.08	−40.08	16	1.257
CN	−40.08	40.08	10	8.0148
CBL2	40.08	60.08	16	1.257
U DP KB25	60.08	70.08	4	2.532

**Table A.19**

Assembly 12A-13-01/2 platelets boundaries.

Plate	From, cm	To, cm	ele. height, cm
Cell U DP KB25			
U DEPL KB25	0	2.5320	2.5320
Cell CBL1			
U NAT KP3	0	0.3138	0.3138
AL 25% KP3	0.3138	0.6290	0.3152
SODIUM KP6	0.6290	1.2570	0.6280
Cell CN			
SODIUM KP6	0	0.6280	0.6280
AL 40% KP3	0.6280	0.9440	0.3160
U 35% KP3	0.9440	1.2574	0.3134
U NAT KP3	1.2574	1.5712	0.3138
SODIUM KP6	1.5712	2.1992	0.6280
U 35% KP3	2.1992	2.5126	0.3134
SODIUM KP6	2.5126	3.1406	0.6280
AL 40% KP3	3.1406	3.4566	0.3160

**Table A.19 (continued)**

Plate	From, cm	To, cm	ele. height, cm
U 35% KP3	3.4566	3.7700	0.3134
AL 40% KP3	3.7700	4.0860	0.3160
U DEPL KP1.5	4.0860	4.2430	0.1570
U NAT KP3	4.2430	4.5568	0.3138
AL 40% KP3	4.5568	4.8728	0.3160
U 35% KP3	4.8728	5.1862	0.3134
SODIUM KP6	5.1862	5.8142	0.6280
AL 40% KP3	5.8142	6.1302	0.3160
U 35% KP3	6.1302	6.4436	0.3134
U NAT KP3	6.4436	6.7574	0.3138
SODIUM KP6	6.7574	7.3854	0.6280
U 35% KP3	7.3854	7.6988	0.3134
AL 40% KP3	7.6988	8.0148	0.3160

**Appendix A.7. Assembly 12A-10-26 - Small slump-in configuration**

This fuel assembly is designated for simulation of small fuel slump-in in the center of the core. As it can be seen in Fig. A.26 and A.27, the fuel is being compacted in the center, while on both sides a voided region (simulated by empty steel cans) is formatted. The rest of the fuel assembly is similar to assembly 12A-10-01 with a single modification, replacement of the sodium plates by voided steel boxes. The dimensions are summarized in Tables A.20 and A.21 with the material balance shown in Table A.22.



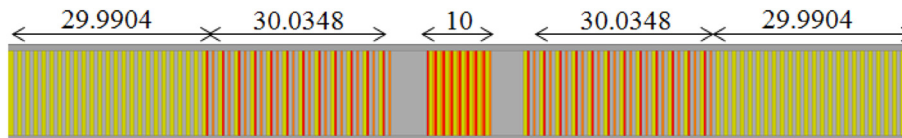


Fig. A.26 Axial cross section of small slump in configuration.

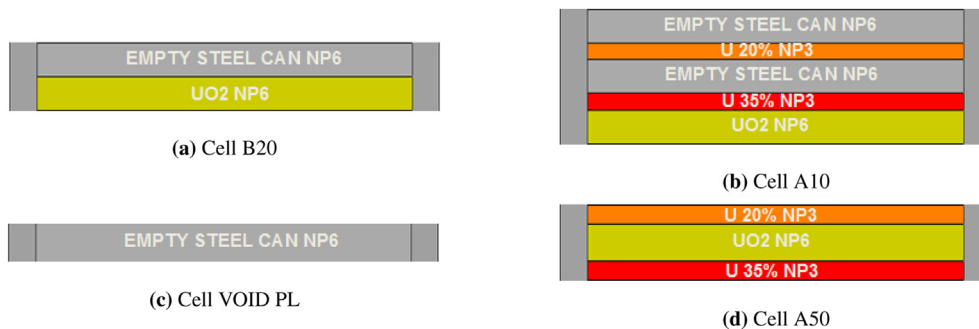


Fig. A.27 Composing cells of assemblies 12A-10-26.

**Table A.20**

Assembly 12A-10-26 cell boundaries and platelets quantities.

Cell	From, cm	To, cm	Num. of ele.	ele. height, cm
B20	−70.0368	−40.0464	24	1.2496
A10	−40.0464	−10.0116	12	2.5029
VOID-PL	−10.0116	−5.0204	8	0.6239
A50	−5.0204	5.0204	8	1.2551
VOID-PL	5.0204	10.0116	8	0.6239
A10	10.0116	40.0464	12	2.5029
B20	40.0464	−70.0368	24	1.2496

**Table A.21**

Assembly 12A-10-26 platelets boundaries.

Plate	From, cm	To, cm	ele. height, cm
Cell VOID PL			
EMPTY STEEL CAN NP6	0	0.6239	0.6239
Cell B20			
UO2 NP6	0	0.6257	0.6257
EMPTY STEEL CAN NP6	0.6257	1.2496	0.6239
Cell A10			
UO2 NP6	0	0.6257	0.6257
U 35% NP3	0.6257	0.9401	0.3144
EMPTY STEEL CAN NP6	0.9401	1.5640	0.6239
U 20% NP3	1.5640	1.8790	0.3150
EMPTY STEEL CAN NP6	1.8790	2.5029	0.6239
Cell A50			
U 35% NP3	0	0.3144	0.3144
UO2 NP6	0.3144	0.9401	0.6239
U 20% NP3	0.9401	1.2551	0.3150

**Table A.22**

Assembly 12A-12-01 material balance, #/ cm b.

Isotop	UO2 NP6	U35% NP3	EMPTY STEEL CAN NP6	U 20% NP3
Al	1.380427E-05	—	—	—
C	6.399417E-05	—	3.34349E-05	—
Cr	1.944067E-03	—	2.18587E-03	—
Fe	6.886453E-03	—	7.62764E-03	—
H	1.765199E-05	—	—	—
Mg	6.123131E-06	—	—	—
Mn	4.007326E-05	—	3.82865E-05	—
Mo	1.126957E-05	—	1.66099E-05	—
Na	—	—	—	—
Nb	5.553869E-07	—	—	—
Ni	1.018455E-03	8.092385E-04	1.45817E-03	8.077022E-04
O	3.990924E-02	—	—	—
P	2.768817E-05	—	1.21425E-04	—
S	1.054332E-06	—	4.17887E-06	—
Si	8.818426E-05	—	1.49793E-04	—
U235	1.432592E-04	1.689311E-02	—	9.292719E-03
U238	1.975188E-02	3.001687E-02	—	3.706167E-02

**Appendix A.8. Assembly 12A-10-27 - Small slump-in configuration**

The fuel assembly 12A-10-27 aim is to simulate large slump in, shown in Fig. A.28, where assembly configuration is summarized in Table A.23. The cell dimensions can be taken from Table A.21 and material distribution from Table A.22.

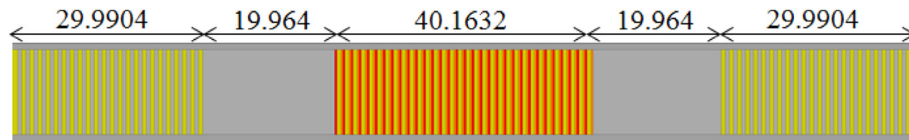


Fig. A.28 Axial cross section of large slump in configuration.

**Table A.23**

Assembly 12A-10-27 cell boundaries and platelets quantities.

Cell	From, cm	To, cm	Num. of ele.	ele. height, cm
B20	−70.0368	−40.0464	24	1.2496
VOID-PL	−40.0464	−20.0816	32	0.6239
A50	−20.0816	20.0816	32	1.2551
VOID-PL	20.0816	40.0464	32	0.6239
B20	40.0464	70.0368	24	1.2496

**Appendix A.9. Assembly 12A-10-96 - Small slump-in configuration**

The last configuration in the SNEAK-12A that would be observed here is the one simulation molten pool. The material composition can be taken from Table A.22 and most of the composing cells (A50, B20 and Empty Steel Cans) can be found in the definition of assembly 12A-10-26 (small slump-in). The assembly 12A-10-96 can be seen in Fig. A.30. The molten pool configuration contains additional cell, that wasn't introduced previously, it is brought in Fig. A.30. The material balance for SUPPORT CAN NP6 is given in Table A.26.

**Table A.25**

Assembly 12A-10-26 platelets boundaries.

Plate	From, cm	To, cm	ele. height, cm
Cell ST FLAME L			
SUPPORT CAN NP6	0	83.51	83.51
Cell B20			
UO2 NP6	0	0.6257	0.6257
EMPTY STEEL CAN NP6	0.6257	1.2496	0.6239
Cell B10			
UO2 NP6	0	0.6257	0.6257
U 35% NP3	0.6257	0.9401	0.3144
UO2 NP6	0.9401	1.5657	0.6257
U 20% NP3	1.5657	1.8808	0.3150
UO2 NP6	1.8808	2.5065	0.6257
Cell A50			
U 35% NP3	0	0.3144	0.3144
UO2 NP6	0.3144	0.9401	0.6239
U 20% NP3	0.9401	1.2551	0.3150

**Table A.26**

Material balance of the empty steel support can, #/ cm b.

Isotop	SUPPORT CAN NP6
Fe	2.90200E-03
Si	4.65000E-05
Mn	3.54000E-05
Cr	8.08600E-04
Ni	3.59900E-04



Fig. A.29 Axial cross section of molten pool configuration.

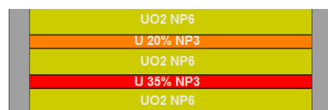


Fig. A.30 Cell B10.

**Table A.24**

Assembly 12A-10-96 cell boundaries and platelets quantities.

Cell	From, cm	To, cm	Num. of ele.	ele. height, cm
ST FLAME L	−73.5000	10.0100	1	83.510
A50	10.0100	40.1324	32	1.2551
B10	40.1324	60.1844	8	2.5065
B20	60.1844	70.1812	8	1.2496

**Appendix A.10. Cladding**

All the assemblies have the same cladding compositions, which is given in Table A.27.

**Table A.27**

Material balance for the assemblies steel cladding, #/ cm b.

Isotop	CLADDING
C	4.0132580E-04
Fe	1.1703970E-01
Cr	3.2792630E-02
Mn	2.5873660E-03
Mo	2.9504490E-04
Nb	2.5284660E-04
Ni	1.6936410E-02
Si	1.3411650E-03

**Appendix A.11. Basic core loading for the presented experiments**

The basic loading pattern for the experiments presented in this paper is shown in Fig. A.31. The core includes all the assemblies

presented in the appendix. However, in order to determine the positions of the different experimental configuration involving material redistribution (e.g. molten pool, slump-in, etc.) it is required to review Figs. 3 and 5.

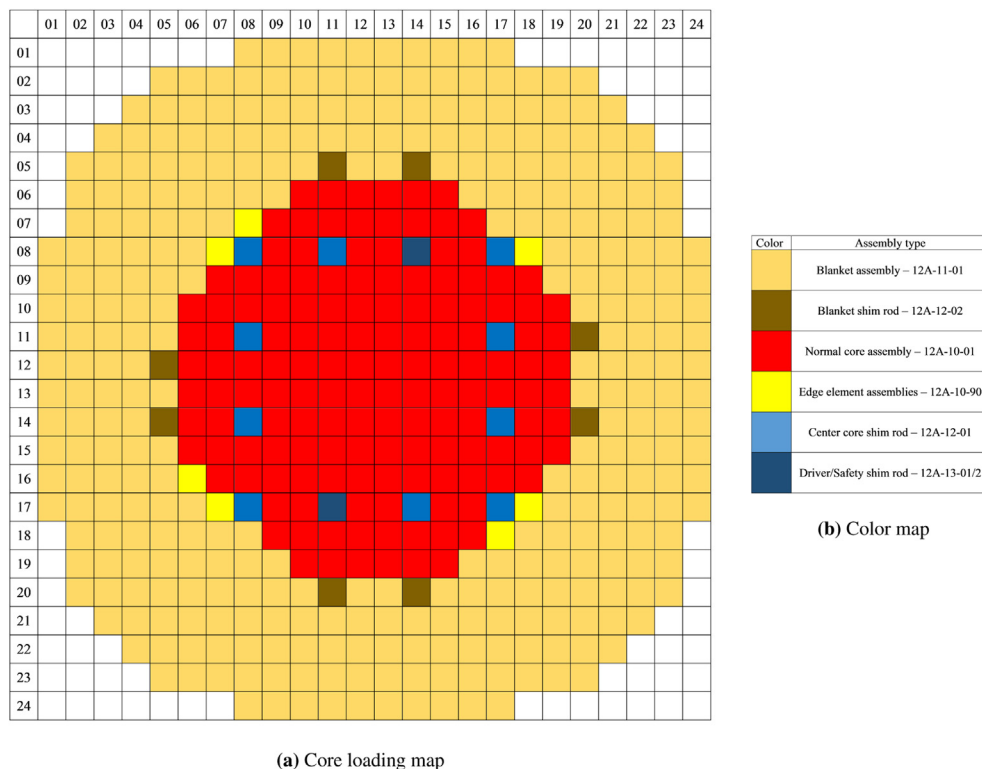


Fig. A.31 Basic SNEAK-12A core loading for all the experimental configuration.

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